

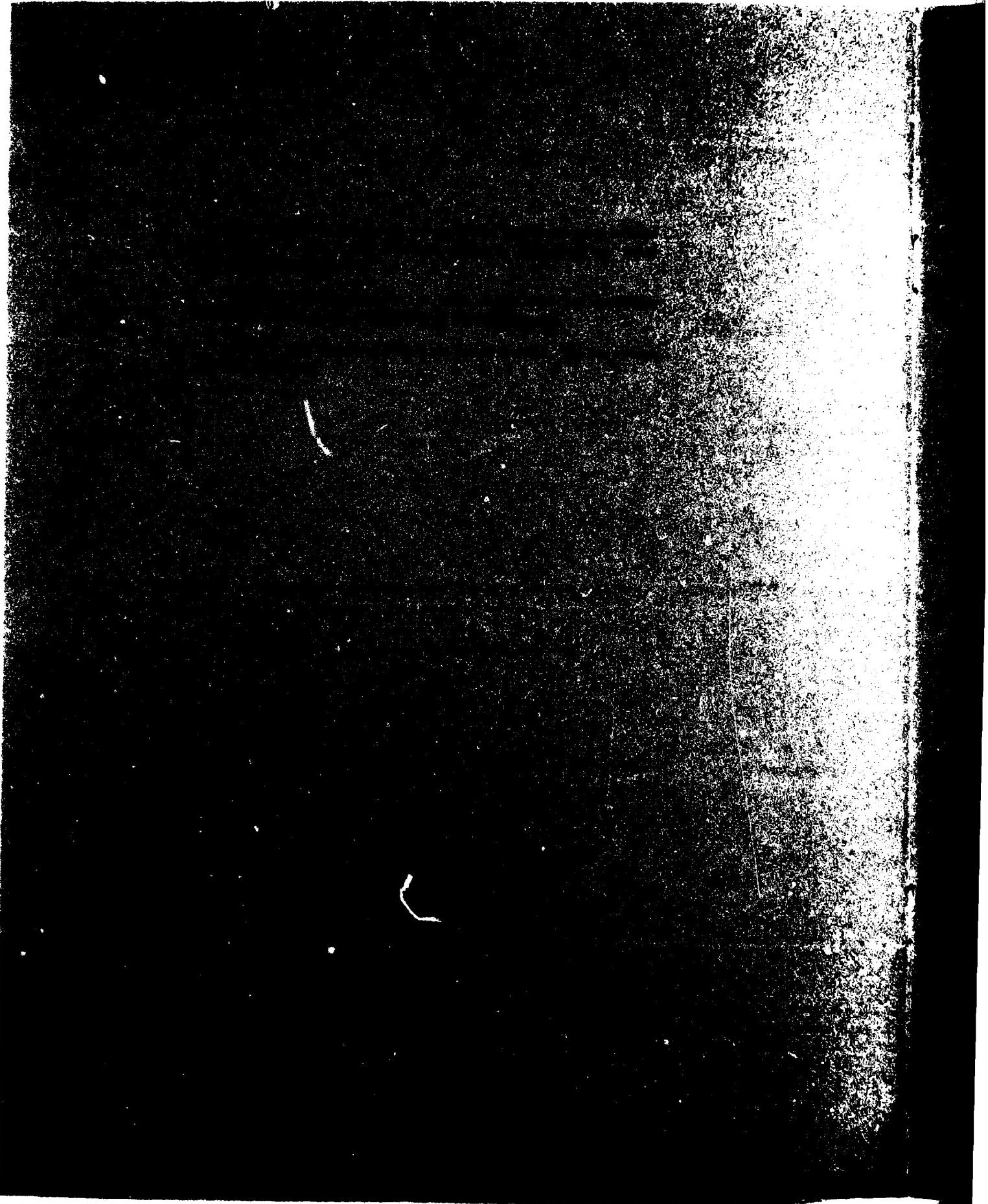
AD-A101 581 HARRY DIAMOND LABS ADELPHI MD F/G 9/1
BIPOLAR TRANSISTOR AND DIODE FAILURE TO ELECTRICAL TRANSIENTS----ETC(U)
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21. ABSTRACT (Continue on reverse side if necessary and identify by block number) An investigation of the predictive capability of a new Air Force Weapons Laboratory model for transistor and diode failure under reverse bias was initiated. A comparison with the junction capacitance damage model shows a doubled improvement at high confidence levels based on an Army-generated population of experimental damage data.		

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1. INTRODUCTION

A recent Air Force Weapons Laboratory (AFWL) document, Electronic Component Modeling and Testing Program, AFWL-TR-78-62 Pt.1 (March 1980), contains a new model for predicting bipolar transistor and diode failure for reverse junction bias. This paper examines the capability of this model using as a baseline a library of experimental damage data for devices from the front ends of an array of Army tactical multichannel radios.

2. EXAMINATION

The new model is implemented as follows:

- (1) Calculate doping concentration from room temperature breakdown voltage:

$$N_D = 4.49 \times 10^{18} V_{BD}^{-1.5}$$

where

N_D = doping concentration on lightly doped side of junction
(inverse cubic centimeters),

V_{BD} = room temperature breakdown voltage (volts).

- (2) Calculate breakdown voltage at critical failure temperature:

$$V_{BDC} = 4.07 \times 10^{12} N_D^{-0.67}$$

where

V_{BDC} = breakdown voltage at critical failure temperature
(volts).

- (3) Calculate space charge resistivity:

$$\rho_{SC} = 2.48 \times 10^{25} N_D^{-1.8}$$

where

ρ_{SC} = space charge resistivity (ohm-square centimeters).

(4) Calculate bulk resistivity:

$$\rho_{BLK} = 3.61 \times 10^{10} N_D^{-0.81},$$

where

ρ_{BLK} = bulk resistivity (ohm-square centimeters).

(5) Calculate failure current density at 100 ns:

Emitter-to-base junction:

$$J_F = 3.84 \times 10^{-11} N_D^{0.88},$$

where

J_F = failure current density at 100 ns (amperes/square centimeter).

Collector-to-base or diode junction:

$$J_F = 8.25 \times 10^{-11} N_D^{0.88}.$$

(6) Calculate junction area:

Emitter-to-base junction:

Priority 1

$$\text{Area} = 1.47 \left(2.3 \times 10^{-6} C_{O_{EB}} V_{BD}^{0.67} \right)^{1.05},$$

where

$C_{O_{EB}} = C_{RE RF}^{0.5}$ = corrected emitter-to-base capacitance (picofarads),

C_{RE} = emitter-to-base capacitance at rated voltage
(picofarads),

V_{RF} = rated voltage (volts),

V_{BD} = rated emitter-to-base breakdown voltage (volts).

Priority 2

$$\text{Area} = 6.34 \times 10^{-4} I_{MAX}^{0.82},$$

where

I_{MAX} = maximum rated transistor collector current (amperes).

Priority 3

$$\text{Area} = 8.75 \times 10^{-3} \left(2 \times 10^{-6} C_{OCB} V_{BD_{CB}}^{0.83} \right)^{0.58},$$

where

$C_{OCB} = C_{RC} V_{RC}^{0.333}$ = corrected collector-to-base capacitance
(picofarads),

C_{RC} = collector-to-base capacitance at rated voltage
(picofarads),

V_{RC} = rated voltage for collector-to-base capacitance (volts),

$V_{BD_{CB}}$ = collector-to-base breakdown voltage (volts).

Priority 4

$$\text{Area} = 1.19 \times 10^{-2} \theta_{JC}^{-0.94},$$

where

θ_{JC} = junction-to-case thermal resistance (degrees Celsius/watt).

Priority 5

$$\text{Area} = 2.79 \theta_{JA}^{-1.70},$$

where

θ_{JA} = junction-to-ambient thermal resistance (degrees Celsius/watt).

Collector-to-base junction:

Priority 1

$$\text{Area} = 0.0470 \frac{1}{\theta_{JC}}^{0.89} .$$

Priority 2

$$\text{Area} = 2.72 \times 10^{-3} I_{MAX}^{0.62} .$$

Priority 3

$$\text{Area} = 3.630 \frac{1}{\theta_{JA}}^{1.47} .$$

Priority 4

$$\text{Area} = 1.13 \times 10^{-2} \left(2 \times 10^{-6} C_{O_{CB}} V_{BD}^{0.83} \right)^{0.39} .$$

Diode junction:

Priority 1

$$\text{Area} = 8.1 \times 10^{-3} I_{MAX}^{1.16} .$$

where

I_{MAX} = maximum rated diode currents (amperes) for Zener diodes
 $= I_{ZM} V_Z$,

I_{ZM} = maximum rated Zener current (amperes),

V_Z = rated Zener voltage (volts).

Priority 2

$$\text{Area} = 0.458 \left(2 \times 10^{-6} C_{O_D} V_{BD}^{0.83} \right)^{0.83} ,$$

where

$$C_{O_D} = C_{RD} V_{RD}^{0.333} ,$$

C_{RD} = diode junction capacitance at rated voltage (picofarads),

V_{RD} = rated voltage (volts).

Priority 3

$$\text{Area} = 0.4890 \frac{-1.21}{\text{JL}} ,$$

where

θ_{JL} = junction-to-lead thermal resistance (degrees Celsius/watt).

Priority 4

$$\text{Area} = 1.9630 \frac{-1.32}{\text{JA}} .$$

(7) Calculate bulk resistance, space charge resistance, and failure current at 100 ns:

$$R_{\text{BLK}} = \rho_{\text{BLK}} / \text{area} ,$$

$$R_{\text{SC}} = \rho_{\text{SC}} / \text{area} ,$$

$$I_F \text{ 100 ns} = J_F X \text{ area} .$$

(8) Calculate power to damage for pulse duration t :

$$P_D = \left[V_{\text{BDC}} \frac{I_F \text{ 100 ns}}{3.162} + \frac{I_F^2 \text{ 100 ns}}{10} (R_{\text{SC}} + R_{\text{BLK}}) \right] / 1000 t^{0.5} .$$

3. RESULTS

Appendix A lists a program used to implement the AFWL model, along with the input and resultant data. The model predictions are presented in figure 1 as

$$P_X / P , \text{ for } P_X \geq P ,$$

$$P / P_X , \text{ for } P > P_X ,$$

where

P_X = experimental power to damage,

P = corresponding predicted value,

as a function of the percentage confidence level. The percentage confidence level is defined as the percentage of data points with a ratio less than or equal to the given value. The envelope defined by the five priority models is plotted in figure 2 along with the predictions of the junction capacitance damage model for comparison and a plot of the scatter in the experimental data. The scatter in the experimental data is the ratio of the power to damage for the individual devices and the experimentally defined damage curve presented in the mode previously indicated for the AFWL model predictions. The experimental data base used for this projection includes but is larger than that indicated in appendix A. The total base of 822 devices comprised a test population of 82 P-N junction types. This population includes both germanium devices and specialty devices for which AFWL model data are unavailable.

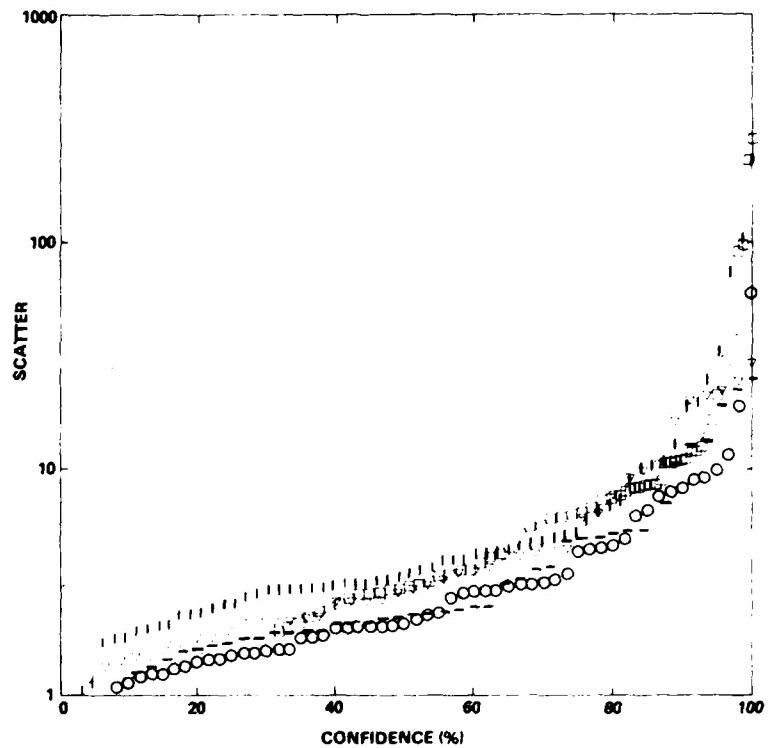


Figure 1. Percentage confidence level versus scatter in data for AFWL model: 0 = priority 1, □ = priority 2, ▽ = priority 3, | = priority 4, and - = priority 5.

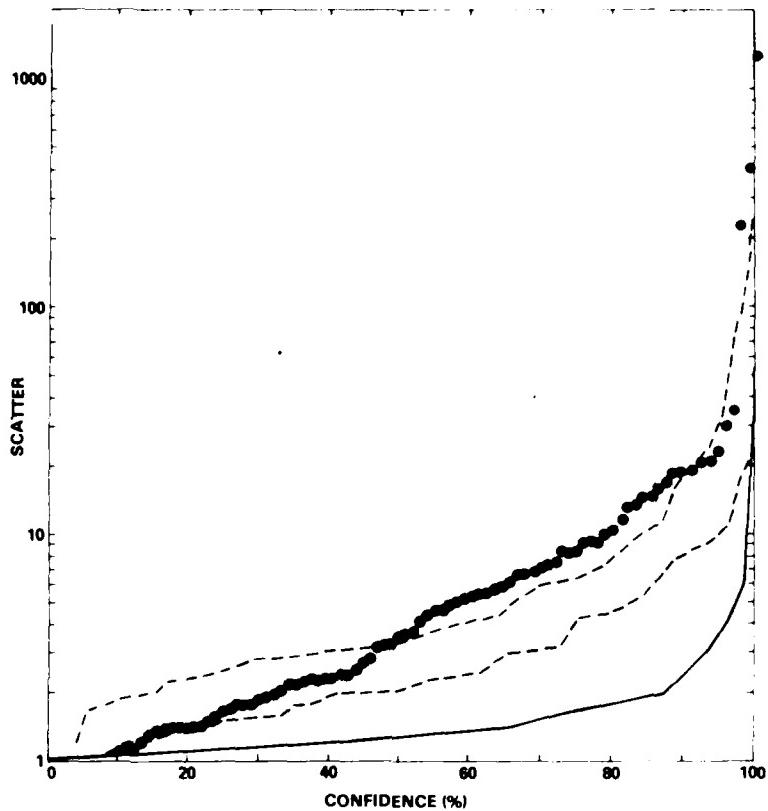


Figure 2. Percentage confidence level versus scatter in data for junction capacitance damage model (solid circles), limits of AFWL damage model (dashed curve), and experimental data (solid curve).

4. CONCLUSION AND DISCUSSION

At high confidence levels, the AFWL model represents approximately a doubled improvement over the junction capacitance damage model based on the device population employed in this study. One note of caution: The AFWL model, like all previous damage models, is for junction reverse bias only. To project from reverse bias failure to failure under forward bias is fraught with great difficulties. Figure 3 is a histogram of the experimental ratio of power to failure for forward and for reverse bias. (All measurements were made at 0.1-, 1-, and 10- μ s pulse durations.) Previous studies have shown that, despite the generally higher power to failure for forward bias, damage is as likely

to occur under forward as under reverse conditions for circuits driven to the failure level.^{1,2} The uncertainty indicated in figure 3 must be included in the uncertainty of the damage model predictions in projecting damage characteristics to forward bias.

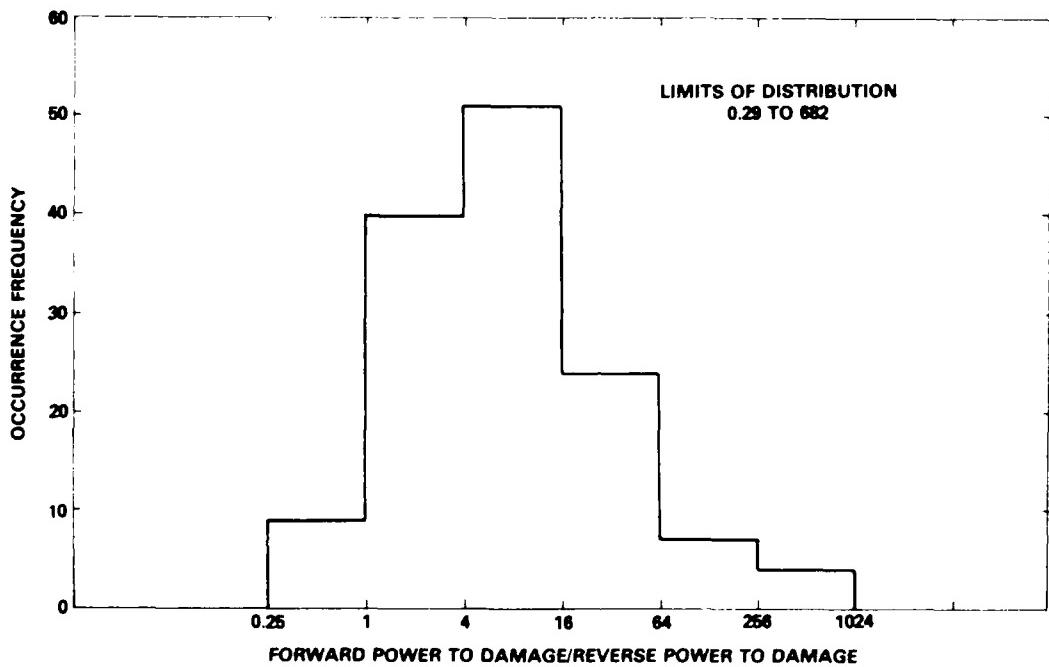


Figure 3. Histogram of ratio of experimental power to damage for forward and reverse junction bias for pulse durations in 0.1- to 10- μ s range for 78 percent of P-N junction types included in appendix A.

¹Michael J. Vrabel, *EMP Assessment for Army Tactical Communications Systems: Transmission Systems Series No. 3 Radio Terminal Sets AN/TRC-112 and AN/TRC-121 (U)*, Harry Diamond Laboratories HDL-TR-1807 (May 1977). (*SECRET-RESTRICTED DATA*)

²George Gornak et al, *EMP Assessment for Army Tactical Communications Systems: Transmission Systems Series No. 1 Radio Terminal Set AN/TRC-145 (U)*, Harry Diamond Laboratories HDL-TR-1746 (February 1976). (*SECRET-RESTRICTED DATA*)

APPENDIX A.--AIR FORCE WEAPONS LABORATORY MODEL CODE, INPUT DATA, AND
RESULTS OF PREDICTING BIPOLAR TRANSISTOR AND DIODE FAILURE
FOR REVERSE JUNCTION BIAS

APPENDIX A

```

C DAT(1,N)=-1= DIODE JUNCTION, 0= C-B JUNCTION, 1= E-B JUNCTION
C DAT(2,N)=BREAKDOWN VOLTAGE (V)
C DAT(3,N)= DIODE CAPACITANCE (PF), DEFAULT VALUE=0
C DAT(4,N)=C-B CAPACITANCE, DEFAULT VALUE=0
C DAT(5,N)= E-B CAPACITANCE (PF), DEFAULT VALUE=0
C DAT(6,N)=MAXIMUM RATED COLLECTOR OR DIODE CURRENT(A)
C DAT(7,N)=JUNCTION-TO -CASE THERMAL RESISTANCE(THETA JC) (C/W)
C DAT(8,N)=JUNCTION-TO-AMBIENT THERMAL RESISTANCE(THETA JA) (C/W)
C DAT(9,N)=BREAKDOWN VOLTAGE FOR C-B FOR EMITTER DATA
C DAT(10,N)=EXPERIMENTAL POWER TO DAMAGE AT 0.1US
C DAT(11,N)=EXPERIMENTAL POWER TO DAMAGE AT 1 US
C DAT(12,N)=EXPERIMENTAL POWER TO DAMAGE AT 10 US
    DIMENSION DAT(12,68), DOPE(68), BV(68), RHOSC(68), RHUBLK(68)
    DIMENSION FAILI(68), AREA(5,68), RBLK(5,68), RSC(5,68), CUR(5,68)
    DIMENSION D(5,68), RATIO(5,3,68), BIG(5), MZ(5), NZ(5), SET(5)
    DIMENSION B(5,150), C(5,150), MV(5), RSULT(5,300)
    DIMENSION DEVICE(272), RAT(5,3,68)
    DIMENSION AVG(3,68), BB(200), CC(200), RSLT(400)
    NAMELIST/LISTA/DAT,DEVICE
    READ(5,LISTA)
    WRITE(6,1)
1   FORMAT(20X,10HBREAKDOWN ,10H DIODE ,10H C-B ,
        &10H E-B ,10HCOLL. CURR,10H THETA JC ,10H THETA JA ,
        &10H BV C-B ,10HDAMAGE ,10HDAMAGE ,10HDAMAGE )
    WRITE(6,2)
2   FORMAT(20X,10H VOLTAGE ,10H CAP. ,10H CAP. ,
        &10H CAP. ,10H MAX. ,30X,10H (0.1US) .
        &10H (1.0US) ,10H (10.US) )
    WRITE(6,3)
3   FORMAT(20X,10H (VOLTS) ,10H (PF) ,10H (PF) ,
        &10H (AMP) ,10H (C/WATT) ,10H (C/WATT) ,
        &10H (WATTS) ,10H (WATTS) ,10H (WATTS) ,10H (WATTS) )
    WRITE(6,4)
4   FORMAT(2X)
    DO 201 N=1,65
    M=4*(N-1)+1
    MM=M+1
    MMM=MM+1
    MMMM=MM+1
    WRITE(6,200)DEVICE(M),DEVICE(MM),DEVICE(MMM),DEVICE(MMM)
    &DAT(M,N),M=2,121
200  FORMAT(2X,4A4,8F10.3,3F10.2)
201  CONTINUE
    DO 100 N=1,68
    IF(DAT(2,N).EQ.0.) GO TO 100
    DOPE(N)=(4.49E+18)*DAT(2,N)**(-1.5)
100   CONTINUE
    DO 101 N=1,68
    IF(DOPE(N).EQ.0.) GO TO 101
    BV(N)=(4.07E+12)*(DOPE(N))**(-0.67)
101   CONTINUE
    DO 102 N=1,68
    IF(DOPE(N).EQ.0.) GO TO 102
    RHOSC(N)=(2.48E+25)*(DOPE(N))**(-1.8)
102   CONTINUE
    DO 103 N=1,68
    IF(DOPE(N).EQ.0.) GO TO 103

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APPENDIX A

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RHOBLK(N)={3.61E+10)*(DOPE(N))**(-0.81)
103 CONTINUE
DO 104 N=1,68
IF(DAT(1,N))105,105,106
105 FAILI(N)={8.26E-11)*(DOPE(N))**(0.88)
GO TO 104
106 FAILI(N)={3.84E-11)*(DOPE(N))**(0.88)
104 CONTINUE
DO 107 N=1,68
IF(DAT(1,N))110,109,108
108 AREA(1,N)=1.47*((2.3E-06)*DAT(5,N)*DAT(2,N)**0.67)**1.05
AREA(2,N)={6.34E-04)*(DAT(6,N))**0.82
AREA(3,N)={8.75E-03)*(2.E-06*DAT(4,N)*(DAT(9,N))**0.83)**0.58
IF(DAT(7,N).EQ.0.) GO TO 150
AREA(4,N)={1.19E-2)*(DAT(7,N))**(-0.94)
150 IF(DAT(8,N).EQ.0.) GO TO 107
AREA(5,N)=2.79*DAT(8,N)**(-1.7)
GO TO 107
109 IF(DAT(7,N).EQ.0.) GO TO 151
AREA(1,N)=0.047*(DAT(7,N))**(-0.89)
151 AREA(2,N)={2.72E-03)*(DAT(6,N))**(-0.62)
IF(DAT(8,N).EQ.0.) GO TO 152
AREA(3,N)=3.63*(DAT(8,N))**(-1.47)
152 AREA(4,N)={1.13E-02)*(2.E-06*DAT(4,N)*DAT(2,N)**0.83)**0.39
GO TO 107
110 AREA(1,N)={8.1E-03)*DAT(6,N)**1.16
AREA(2,N)=0.458*(2.E-06*DAT(3,N)*DAT(2,N)**0.83)**0.83
IF(DAT(7,N).EQ.0.) GO TO 153
AREA(3,N)=0.489*DAT(7,N)**(-1.21)
153 IF(DAT(8,N).EQ.0.) GO TO 107
AREA(4,N)=1.963*DAT(8,N)**(-1.32)
107 CONTINUE
DO 111 N=1,68
DO 112 M=1,5
IF(AREA(M,N).EQ.0.) GO TO 112
RBLK(M,N)=RHOBLK(N)/AREA(M,N)
RSC(M,N)=RHOSC(N)/AREA(M,N)
CUR(M,N)=FAILI(N)*AREA(M,N)
112 CONTINUE
111 CONTINUE
DO 116 N=1,68
DO 113 M=1,5
D(M,N)={(BVIN)*(CUR(M,N)/3.162)+(CUR(M,N)**2)/10.)*
E(RSC(M,N)+RBLK(M,N)))/1000.
113 CONTINUE
116 CONTINUE
DO 117 N=1,68
DO 118 M=1,3
DO 114 K=1,5
MM=9+M
AM=M-1
IF(D(K,N).EQ.0.) GO TO 114
RATIO(K,M,N)=DAT(MM,N)/(D(K,N)*3162.*{(10.)*(-0.5*AM)})
RATE(K,M,N)=RATIO(K,M,N)
IF(RATIO(K,M,N).EQ.0.) GO TO 114
IF(RATIO(K,M,N).GE.1.) GO TO 114
RATIO(K,M,N)=1./RATIO(K,M,N)
114 CONTINUE
118 CONTINUE
117 CONTINUE

```

APPENDIX A

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15  WRITE(6,15)
FORMAT(2X//++)
WRITE(6,5)
5   FORMAT(2X,12H RATIO OF EXPERIMENTAL POWER TO DAMAGE TO PREDICTED V
      VALUE FOR 0.1, 1.0, AND 10 USEC PULSE DURATIONS FOR FIVE PRIORITY M
      CODELS//)
WRITE(6,6)
6   FORMAT(26X,12H    PRTY 1    ,12H    PRTY 2    ,12H    PRTY 3    ,
          12H    PRTY 4    ,12H    PRTY 5    /)
DO 312 L=1,3
DO 311 N=1,65
M=4*(N-1)+1
MM=M+1
MMM=MM+1
MMMM=MM+1
WRITE(6,310)DEVICE(M),DEVICE(MM),DEVICE(MMM),DEVICE(MMM),
& (RAT(K,L,N),K=1,5)
310 FORMAT(10X,4A4,5F12.4)
311 CONTINUE
WRITE(6,313)
313 FORMAT(2X//)
312 CONTINUE
DO 800 N=1,68
DO 801 M=1,3
AJ=0.
DO 802 K=1,5
AVG(M,N)=RATIO(K,M,N)+AVG(M,N)
IF(RATIO(K,M,N).EQ.0.) GO TO 802
AJ=1.+AJ
802 CONTINUE
IF(AVG(M,N).EQ.0.) GO TO 801
AVG(M,N)=AVG(M,N)/AJ
801 CONTINUE
800 CONTINUE
DO 803 LL=1,200
DO 804 N=1,68
DO 805 M=1,3
IF(AVG(M,N).EQ.0.) GO TO 805
IF(AVG(M,N).LE.BIGG) GO TO 805
BIGG=AVG(M,N)
MAVG=M
NAVG=N
805 CONTINUE
804 CONTINUE
NZAA=1+NZAA
IF(SETT.EQ.1.) GO TO 806
IF(BIGG.NE.0.) GO TO 806
SETT=1.
MVV=NZAA-1
MAV=MVV
806 CONTINUE
BB(NZAA)=BIGG
BIGG=0.
AVG(MAVG,NAVG)=0.
803 CONTINUE
DO 808 N=1,200
BN=N-1
AMV=MVV
CC(N)=100.-BN*(100./AMV)
808 CONTINUE

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APPENDIX A

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MM=0
DO 880 N=1,MVV
AVERAG=BB(N)+AVERAG
880 CONTINUE
AVERAG=AVERAG/AMV
DO 809 N=1,MVV
MM=1+MM
RSLT(MM)=BB(N)
MM=1+MM
RSLT(MM)=CC(N)
809 CONTINUE
DO 130 LL=1,150
DO 123 N=1,68
DO 124 M=1,3
DO 120 K=1,5
IF(RATIO(K,M,N).EQ.0.) GO TO 120
IF(RATIO(K,M,N).LE.BIG(K)) GO TO 120
BIG(K)=RATIO(K,M,N)
MZ(K)=M
NZ(K)=N
120 CONTINUE
124 CONTINUE
123 CONTINUE
NZA=1+NZA
DO 131 KK=1,5
IF(SET(KK).EQ.1.) GO TO 131
IF(BIG(KK).NE.0.) GO TO 131
SET(KK)=1.
MV(KK)=NZA-1
131 CONTINUE
DO 132 KK=1,5
B(KK,NZA)=BIG(KK)
BIG(KK)=0.
132 CONTINUE
DO 133 KK=1,5
MZZ=MZ(KK)
NZZ=NZ(KK)
RATIO(KK,MZZ,NZZ)=0.
133 CONTINUE
130 CONTINUE
DO 140 N=1,150
DO 135 K=1,5
BN=N-1
AMV=MV(K)
C(K,N)=100.-BN*(100./(AMV+.0000001))
135 CONTINUE
140 CONTINUE
DO 142 K=1,5
MVV=MV(K)
MM=0
DO 141 N=1,MVV
MM=1+MM
RSULT(K,MM)=B(K,N)
MM=1+MM
RSULT(K,MM)=C(K,N)
141 CONTINUE
142 CONTINUE
WRITE(6,11)
11 FORMAT(2X///)
WRITE(6,10)

```

APPENDIX A

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10  FORMAT(12X,128HRATIO EXPERIMENTAL AND PREDICTED POWER TO DAMAGE VS
    PERCENTAGE CONFIDENCE LEVEL FOR ALL PULSE DURATIONS FOR FIVE PRIORITY
    CITY MODELS//)
DO 145 K=1,5
MJV=(MV(K)+1)*2
WRITE(6,146)(RESULT(K,M),M=1,MJV)
146 FORMAT(5X,2F9.2,3X,2F9.2,3X,2F9.2,3X,2F9.2,2X,2F9.2)
WRITE(6,12)
12  FORMAT(12X//)
145 CONTINUE
WRITE(6,810)
810 FORMAT(12X///)
WRITE(6,811)
811 FORMAT(12X,124HRATIO OF EXPERIMENTAL AND PREDICTED POWER TO DAMAGE
    VS PERCENTAGE CONFIDENCE LEVEL FOR AVERAGE VALUE OF FIVE PRIORITY
    EMODELS//)
MJV=(MAV+1)*2
WRITE(6,146)(RSLT(M),M=1,MJV)
WRITE(6,810)
WRITE(6,881) AVERAG
881 FORMAT(15X,31HARITHMETIC MEAN OF ABOVE DATA =,F9.2)
STOP
END
/*
//GD.SYSIN DD *
ELISTA DAT=0,120,0,11,0,.05,0,357,120,140,52,20,
1,33,0,0,9,.05,0,357,120,30,16,9,
0,250,0,16,0,.025,0,0,250,300,80,20,
1,27,0,0,9,.025,0,0,250,100,44,20,
0,54,0,17,0,0,0,1000,54,160,70,30,
1,7,0,0,22,0,0,1000,54,625,112,70,
0,200,0,4,3,0,.05,0,500,200,50,46,42,
1,10,2,0,0,5,3,.05,0,500,200,160,48,15,
0,107,0,142,0,1,5,0,345,107,115,72,44,
1,7,8,0,0,53,1,5,0,345,107,590,255,110,
0,45,0,8,0,.03,0,500,45,180,74,30,
1,5,0,0,0,.03,0,500,45,230,60,16,
0,108,0,57,0,0,0,476,108,10,10,10,
1,7,4,0,0,8,0,0,476,108,53,30,18,
0,93,0,18,0,.6,0,434,93,135,33,20,
1,8,5,0,0,23,.6,0,434,93,110,78,53,
0,107,0,15,0,.8,0,303,107,220,85,32,
1,7,3,0,0,31,.8,0,303,107,400,135,40,
-1,0,0,0,0,1,0,0,0,2800,2300,2100,
-1,0,0,0,0,0,0,0,4100,2700,1600,
-1,.64,0,0,0,0,0,0,0,6400,2700,1400,
-1,2,5,0,0,0,0,0,0,3,4,2,1,1,
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```

APPENDIX A

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4H2N33,4H5(E,-4HB),4H
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4H2N33,4H6:JA,4HN(E,-4HB),4H
4H2N24,4H84(C,4H-B),4H
4H2N24,4H84(E,4H-B),4H
4H2N37,4H36(C,4H-B),4H
4H2N37,4H36(E,4H-B),4H
4H2N93,4H0(C,-4HB),4H
4H2N93,4H0(E,-4HB),4H
4H2N24,4H81(C,4H-B),4H
4H2N24,4H81(E,4H-B),4H
4H2N29,4H07A(,4HC-B),4H
4H2N29,4H07A(,4HE-B),4H
4H2N22,4H22A(,4HC-B),4H
4H2N22,4H22A(,4HE-B),4H
4H1N43,4H84,4H
4HF591,4H1-34,4H65,4H
4H1N81,4H6,4H
4H1N21,4HME,4H
4H1N91,4H4A,4H
4H1N75,4H2A,4H
4HPC11,4H5,4H
4H1N30,4H26B:,4HJAN,4H
4H1N36,4H11,4H
4H1N39,4H95A,4H
4H1N30,4H16B,4H
4H1N41,4H41,4H

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APPENDIX A

4H1002,4H ,4H ,4H *
4H2N28,4H57(C,4H-B) ,4H *
4H2N28,4H57(E,4H-B) ,4H *
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4H2N33,4H75(E,4H-B) ,4H *
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4H2N14,4H90:J,4HAN(E,4H-B) *
4H2N35,4H84(C,4H-B) ,4H *
4H2N35,4H84(E,4H-B) ,4H *
4H2N28,4H94(C,4H-B) ,4H *
4H2N28,4H94(E,4H-B) ,4H *
4H2N58,4H29(C,4H-B) ,4H *
4H2N58,4H29(E,4H-B) ,4H *
4H2N30,4H13:J,4HAN(C,4H-B) *
4H2N30,4H13:J,4HAN(E,4H-B) *
4HCA30,4H18(C,4H-B) ,4H *
4HCA30,4H18(E,4H-B) ,4H *
4H2N16,4H13:J,4HAN(C,4H-B) *
4H2N16,4H13:J,4HAN(E,4H-B) *
4H2N14,4H85:J,4HAN(C,4H-B) *
4H2N14,4H85:J,4HAN(E,4H-B) *
4H2N34,4H39(C,4H-B) ,4H *
4H2N34,4H39(E,4H-B) ,4H *
4H2N70,4H6:JA,4HN(C-,4HB) *
4H2N70,4H6:JA,4HN(E-,4HB) *
4H1N25,4H80 ,4H ,4H *
4H1N75,4H1A:J,4HAN ,4H *
4H1N48,4H5B:J,4HAN ,4H *
4H1N29,4H91B: 4HJAN ,4H *
4H1N30,4H25E: ,4HJAN ,4H *
4HM010,4H54 ,4H ,4H *
4H1N74,4H6A:J,4HAN ,4H *
4H1N64,4H5:JA,4HN ,4H *
4H1N12,4H02RA,4H:JAN,4H *
4H1N17,4H31A: ,4HJAN ,4H *
EEND.
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APPENDIX A

BREAKDOWN VOLTAGE (VOLTS)	DIODE CAP. (PF)	C-B CAP. (PF)	F-B CAP. (PF)	COLL. CURR. MAX. (AMPS)	THETA JC (C/WATT)	THETA JA (C/WATT)	BV C-E (0.1USS) (WATTS)	DAMAGE (0.1USS) (WATTS)	DAMAGE (10.USS) (WATTS)
2N320A(C-B)	120.000	0.0	11.000	0.0	-0.050	0.0	357.000	120.000	140.00
2N320A(E-B)	33.000	0.0	9.000	0.0	0.050	0.0	357.000	120.000	16.00
2N335(C-B)	250.000	0.0	16.000	0.0	0.025	0.0	250.000	300.000	80.00
2N335(E-B)	27.000	0.0	0.0	9.000	0.025	0.0	250.000	100.000	44.00
2N336:JAN(C-B)	54.000	0.0	17.000	0.0	0.0	0.0	1000.000	54.000	160.00
2N336:JAN(E-B)	7.000	0.0	0.0	22.000	0.0	0.0	1000.000	54.000	70.00
2N2084(C-B)	200.000	0.0	4.300	0.0	0.050	0.0	500.000	200.000	50.00
2N2084(E-B)	10.200	0.0	0.0	5.300	0.050	0.0	500.000	200.000	48.00
2N2074(C-B)	107.000	0.0	142.000	0.0	1.500	0.0	345.000	107.000	115.00
2N2074(E-B)	7.800	0.0	0.0	53.000	1.500	0.0	345.000	107.000	72.00
2N301(C-B)	45.000	0.0	8.000	0.0	0.030	0.0	45.000	180.00	255.00
2N301(E-B)	7.000	0.0	0.0	0.0	0.030	0.0	500.000	45.000	110.00
2N2481(C-B)	108.000	0.0	57.000	0.0	0.0	0.0	476.000	108.000	110.00
2N2481(E-B)	7.400	0.0	0.0	8.000	0.0	0.0	476.000	108.000	15.00
2N2907A(C-B)	93.000	0.0	18.000	0.0	0.600	0.0	434.000	93.000	53.00
2N2907A(E-B)	6.500	0.0	0.0	23.000	0.600	0.0	434.000	93.000	20.00
2N2222A(C-B)	107.000	0.0	15.000	0.0	0.800	0.0	303.000	107.000	78.00
2N2222A(E-B)	7.300	0.0	0.0	31.000	0.800	0.0	303.000	107.000	53.00
1N6384	0.0	0.0	0.0	0.0	1.000	0.0	0.0	0.0	30.00
F5911-34665	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10.00
1N816	0.640	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.00
1N21UE	2.500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1N916A	115.000	0.0	5.700	0.0	0.075	0.0	203.000	107.000	220.00
1N752A	15.700	40.000	0.0	0.0	0.0	0.0	0.0	0.0	32.00
PC115	154.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	15.00
1N3026B:JAN	18.000	2320.000	0.0	0.0	0.0	0.0	0.0	0.0	210.00
1N3611	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1600.00
1N3995A	4.700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1400.00
1N3016B	6.800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.10
1N6141	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1002	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2N2571(C-B)	40.000	0.0	1.000	0.0	0.040	0.0	132.000	40.000	17000.00
2N2571(E-B)	5.400	0.0	0.0	0.0	0.040	0.0	909.000	909.000	17000.00
2N3375(C-B)	87.000	0.0	0.0	0.0	0.0	0.0	3000.00	3000.00	3000.00
2N3375(E-B)	6.000	0.0	0.0	0.0	0.0	0.0	3000.00	3000.00	6224.00
2N1490:JAN(C-B)	120.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13000.00
2N1490:JAN(E-B)	14.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	13000.00
2N3584(C-B)	315.000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	315.000
2N3584(E-B)	9.100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	10000.00
2N2694(C-B)	36.000	0.0	6.000	0.0	0.200	0.0	500.000	170.000	2150.00
2N2694(E-B)	6.400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	150.00
CA3018(C-B)	7.100	0.0	0.0	0.0	0.600	0.050	0.0	200.000	53.000
CA3018(E-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	14.00
2N5229(C-B)	30.000	0.0	0.800	0.0	0.030	0.0	909.000	30.000	47.00
2N5229(E-B)	3.000	0.0	0.0	0.0	0.030	0.0	909.000	30.000	22.00
2N3013:JAN(C-B)	40.000	0.0	5.000	0.0	0.200	0.0	500.000	40.000	100.00
2N3013:JAN(E-B)	5.000	0.0	0.0	0.0	0.200	0.0	500.000	40.000	21.00
CA3018(C-B)	53.000	0.0	0.0	0.0	0.580	0.050	0.0	200.000	53.000
CA3018(E-B)	7.100	0.0	0.0	0.0	0.600	0.050	0.0	200.000	53.000
2N1613:JAN(C-B)	123.000	0.0	25.000	0.0	0.500	0.0	222.000	123.000	2100.00
2N1613:JAN(E-B)	8.800	0.0	0.0	0.0	0.500	0.0	222.000	123.000	160.00
2N1685:JAN(C-B)	205.000	0.0	0.0	0.0	3.000	0.0	0.0	205.000	1700.00
2N1685:JAN(E-B)	16.000	0.0	0.0	0.0	3.000	0.0	0.0	205.000	1100.00
2N339(C-B)	575.000	0.0	0.0	0.0	1.000	0.0	0.0	29000.00	30000.00
2N339(E-B)	9.400	0.0	0.0	0.0	1.000	0.0	0.0	2200.00	78.00
2N706:JAN(C-B)	25.000	0.0	0.0	0.0	0.0	0.0	0.0	25.000	17.00
2N706:JAN(E-B)	5.000	0.0	0.0	0.0	0.0	0.0	0.0	25.000	6.80

IN2580	536.000	0.0	0.0	0.0	12.000	0.0	0.0	0.0	170000.00	53720.00	17000.00
IN151A:JAN	5.100	265.000	0.0	0.0	0.0	0.0	0.0	0.0	25500.00	2500.00	240.00
IN6580:JAN	270.000	6.000	0.0	0.0	0.200	0.0	0.0	0.0	2000.00	435.00	100.00
IN2991B:JAN	36.000	730.000	0.0	0.0	0.0	0.0	0.0	0.0	100000.00	31600.00	10000.00
IN4025B:JAN	16.000	310.000	0.0	0.0	0.0	0.0	0.0	0.0	14000.00	14000.00	1400.00
NO1054	505.000	85.000	0.0	0.0	0.0	0.0	0.0	0.0	40.00	33.50	25.00
IN746A:JAN	3.200	350.000	0.0	0.0	0.0	0.0	0.0	0.0	153800.00	20000.00	2600.00
IN6452:JAN	725.000	17.000	0.0	0.0	0.400	0.0	0.0	0.0	1625.00	580.00	500.00
IN1202R:JAN	514.000	0.0	0.0	0.0	12.000	0.0	0.0	0.0	9000.00	1000.00	100.00
IN1731A:JAN	1580.000	0.0	0.0	0.0	0.350	0.0	0.0	0.0	5700.00	2000.00	800.00

RATIO OF EXPERIMENTAL POWER TO DAMAGE TO PREDICTED VALUE FOR 0.1, 1.0, AND 10 USEC PULSE DURATIONS FOR FIVE PRIORITY MODELS

	PRTY 1	PRTY 2	PRTY 3	PRTY 4	PRTY 5
2N3280:(C-B)	0.0	0.4908	0.3246	0.2566	0.0
2N3281:(E-B)	0.2935	1.1214	0.0	0.0	0.6775
2N3285:(C-B)	0.0	2.1016	0.0	0.4670	0.0
2N335(E-B)	1.0246	6.0125	0.0	0.0	0.0
2N336:JAN(C-B)	0.0	0.0	1.2035	0.2287	0.0
2N336:JAN(E-B)	2.7970	0.0	0.0	0.0	22.5051
2N2480:(C-B)	0.0	0.2111	0.2291	0.1349	0.0
2N2680:(E-B)	3.2438	3.1116	0.0	0.0	2.3489
2N3730:(C-B)	0.0	0.0688	0.2426	0.0772	0.0
2N3736:(E-B)	1.0583	0.5799	0.0	0.0	3.7889
2N930:(C-B)	0.0	0.5655	0.4471	0.3349	0.0
2N930:(E-B)	0.0	3.4508	0.0	0.0	1.9122
2N2240:(C-B)	0.0	0.0	0.0340	0.0096	0.0
2N2481:(E-B)	0.68%	0.0	0.0	0.0	0.5647
2N2901A:(C-B)	0.0	0.0117	0.3774	0.2006	0.0
2N2901A:(E-B)	0.4763	0.2466	0.0	0.0	1.1137
2N222A:(C-B)	0.0	0.1323	0.3834	0.3547	0.0
2N222A:(E-B)	1.2536	0.4251	0.0	0.0	1.9563
1N4386	0.0	0.0	0.0	0.0	0.0
F5911-3465	0.0	0.0	0.0	0.0	0.0
1N816	0.0	0.0	0.0	0.0	0.0
1N214C	0.0	0.0	0.0	0.0	0.0
1N914A	1.5322	0.6474	0.0	0.0	0.0
1N752A	0.0	0.7561	0.0	0.0	0.0
PC115	0.0	0.0	0.0	0.0	0.0
1N3020B:JAN	0.0	2.4439	0.0	0.0	0.0
1N3461	0.0	0.0	0.0	0.0	0.0
1N214C	0.0	0.0	0.0	0.0	0.0
N3995A	0.0	0.0	0.0	0.0	0.0
1N3016B	0.0	0.0	0.0	0.0	0.0
1N4141	0.0	0.0	0.0	0.0	0.0
1D2	0.0	0.0	0.0	0.0	0.0
2N2657:(C-B)	0.0	0.2968	0.46753	0.4912	0.0
2N2657:(E-B)	0.0	0.1162	0.0	0.0	0.2018
2N3375:(C-B)	0.0	0.5569	0.0	0.0	0.0
2N3375:(E-B)	0.0	0.6765	0.0	0.0	0.0
2N1493:JAN(C-B)	0.0	1.0331	0.0	0.0	0.0
2N1493:JAN(E-B)	0.0	1.2612	0.0	0.0	0.0
2N3586:(C-B)	0.0	6.1278	0.0	3.2309	0.0
2N3586:(E-B)	0.0	3.301	0.0	0.0	0.0
2N2094:(C-B)	0.0	4.0991	0.0	3.7194	0.0
	0.0	0.1465	0.3755	0.3383	0.0

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2N2094 (E-B)	0.0	0.1313	0.0	0.3090
2N5821 (E-B)	0.0	0.184	0.0	0.1963
2N5821 (E-B)	0.0	0.2229	0.0	0.2253
2N3013:JAN (C-B)	0.0	0.0912	0.0	0.0
2N3013:JAN (C-B)	0.0	0.2337	0.0	0.3058
LA3010 (C-B)	0.0	0.1037	0.0	0.2185
CA3010 (E-B)	0.0	0.1587	0.0	0.0
CA3010 (E-B)	4.3243	0.3267	0.0	0.4323
2N1613:JAN (C-B)	0.0	0.7164	3.7253	0.0
2N1613:JAN (C-B)	0.0	1.9810	0.0	0.0
2N1448:JAN (C-B)	0.0	0.5718	0.0	0.0
2N1448:JAN (C-B)	0.0	2.79	2.683	0.0
2N3439 (C-B)	0.0	0.0728	0.0	0.0
2N3439 (E-B)	0.0	3.4632	0.0	0.0
2N706:JAN (C-B)	0.0	0.0	0.1657	0.0
2N706:JAN (C-B)	0.0	0.0	0.1679	0.0
LN2580	2.9173	0.0	0.0	0.4157
LN751:JAN	0.0	1.6703	0.0	0.0
LN685:JAN	3.1721	0.0	0.0	0.0
LN2998:JAN	0.0	2.2558	0.0	0.0
LN3028:JAN	0.0	3.6068	0.0	0.0
LN3028:JAN	0.0	10.6319	0.0	0.0
401056	0.0	0.0043	0.0	0.0
LN7464:JAN	0.0	6.5441	0.0	0.0
LN645:JAN	1.5848	0.5301	0.0	0.0
LN1202:JA:JAN	0.1526	0.0	0.0	0.0
LN1731:JA:JAN	8.2311	0.0	0.0	0.0
2N328A (C-B)	0.0	0.5765	0.3813	0.0
2N328A (E-B)	0.4950	1.8913	0.0	0.0
2N335 (C-B)	0.0	1.7722	0.0	0.0
2N335 (E-B)	1.4284	8.3658	0.0	0.0
2N336:JAN (C-B)	0.0	0.0	1.6650	0.0
2N336:JAN (E-B)	1.5850	0.0	0.0	0.0
2N2486 (C-B)	0.0	0.6141	0.6664	0.0
2N2486 (E-B)	3.0773	2.9519	0.0	0.0
2N373:J (C-B)	0.0	0.027	0.4803	0.0
2N373:J (E-B)	1.4465	0.7226	0.0	0.0
2N930 (C-B)	0.0	0.7351	0.2812	0.0
2N930 (E-B)	0.0	3.1767	0.0	0.0
2N2481 (C-B)	0.0	0.0	1.075	0.0
2N2481 (E-B)	1.2343	0.0	0.0	0.0
2N2907 (C-B)	0.0	0.1139	0.4685	0.0
2N2907 (E-B)	1.0679	0.5485	0.0	0.0
2N2224 (C-B)	0.0	0.1616	0.4685	0.0
2N2224 (E-B)	1.3380	0.6612	0.0	0.0
LN6386	0.0	0.0	0.0	0.0
F5911-3465	0.0	0.0	0.0	0.0
LN816	0.0	0.0	0.0	0.0
LN214E	0.0	0.0	0.0	0.0
LN914A	0.9229	0.3699	0.0	0.0
LN752A	0.0	0.3535	0.0	0.0
PC115	0.0	0.0	0.0	0.0
LN3028:JAN	0.0	2.4421	0.0	0.0
LN3611	0.0	0.0	0.0	0.0
LN3995A	0.0	0.0	0.0	0.0
LN30168	0.0	0.0	0.0	0.0
LN6161	0.0	0.0	0.0	0.0
10D2	0.0	0.0	0.0	0.0
2N2857 (C-B)	0.0	0.1251	0.2847	0.0

2N28571(E-8)	0.0	0.1165	0.0	0.0
2N33751(C-8)	-0.9819	1.1850	0.0	0.0
2N33751(E-8)	0.0	1.1057	0.0	0.0
2N14905:JAN(C-8)	0.5020	1.3104	0.0	1.0474
2N14905:JAN(E-8)	0.0	5.6643	0.0	0.0
2N35861(C-8)	0.2160	0.3316	0.0	0.0
2N35861(E-8)	0.0	2.7937	0.0	2.5288
2N28941(C-8)	0.0	0.1362	0.0	0.0
2N28941(E-8)	0.0	0.2631	0.0	0.0
2N58291(C-8)	0.0	0.1354	0.0	0.0
2N58291(E-8)	0.0	0.2577	0.0	0.0
2N30132:JAN(C-8)	0.0	0.3205	0.0	0.0
2N30132:JAN(E-8)	0.0	0.0606	0.0	0.0
CA30161(C-8)	0.0	0.3220	0.0	0.0
CA30161(E-8)	6.2216	0.1568	0.0	0.0
2N16132:JAN(C-8)	0.0	0.1568	0.0	0.0
2N16132:JAN(E-8)	0.0	0.4696	0.0	0.0
2N14652:JAN(C-8)	0.0	5.6772	0.0	0.0
2N14652:JAN(E-8)	0.0	7.7308	0.0	0.0
2N34391(C-8)	0.0	2.8485	0.0	0.0
2N34391(E-8)	0.0	1.1699	0.0	0.0
2N34391(C-8)	0.0	91.5512	0.0	74.6255
2N34391(E-8)	0.0	0.0797	0.0	0.0
2N7062:JAN(C-8)	0.0	3.0664	0.0	0.0
2N7062:JAN(E-8)	0.0	0.0	0.0	0.0
IN2580	0.0	0.0	0.0	0.0
IN751A:JAN	0.0	0.5178	0.0	0.0
IN685R:JAN	2.1818	1.5309	0.0	0.0
IN2991B:JAN	0.0	3.6042	0.0	0.0
IN30258:JAN	0.0	3.3621	0.0	0.0
MO1056	0.0	0.0104	0.0	0.0
1N7461:JAN	0.0	2.6111	0.0	0.0
IN643:JAN	1.7887	0.5983	0.0	0.0
1N1202RA:JAN	0.0535	0.0	0.0	0.0
IN1731A:JAN	9.1350	0.0	0.0	0.0
2N3261(C-8)	0.0	0.7011	0.0	0.0
2N32841(E-8)	0.6806	3.3641	0.0	0.0
2N3351(C-8)	1.4651	0.011	0.0	0.0
2N3351(E-8)	2.0532	12.0251	0.0	0.0
2N3361:JAN(C-8)	0.0	0.0	2.2565	0.0
2N3361:JAN(E-8)	0.0	0.0	0.0	0.0
2N24661(C-8)	0.0	1.7731	1.9242	25.2057
2N24661(E-8)	3.0411	2.9171	0.0	0.0
2N37261(C-8)	0.0	1.791	0.9281	2.2021
2N37261(E-8)	1.9731	1.0811	0.0	0.0
2N9301(C-8)	0.0	0.3424	0.7451	2.0440
2N9301(E-8)	0.0	2.6768	0.0	0.0
2N24611(C-8)	0.0	0.0	0.3398	1.3302
2N24611(E-8)	2.3439	0.0	0.0	0.0
2N2907A1(C-8)	0.0	0.1359	0.5591	1.9177
2N2907A1(E-8)	2.2947	1.1785	0.0	0.0
2N2222A1(C-8)	0.0	0.1924	0.5577	5.3658
2N2222A1(E-8)	1.2536	0.6251	0.0	0.0
1N4364	0.0	0.0	0.0	0.0
F5911-3465	0.0	0.0	0.0	0.0
1N616	0.0	0.0	0.0	0.0
1N21BF	0.0	0.0	0.0	0.0
1N916A	0.5432	0.2312	0.0	0.0
1N7524	0.0	0.2729	0.0	0.0
0.02023	0.0	0.0	0.0	0.0

APPENDIX A

PC115	0.0	0.0	0.0	0.0
1N3026E:JAN	0.0	2.4439	0.0	0.0
1N3611	0.0	0.0	0.0	0.0
1N3995A	0.0	0.0	0.0	0.0
1N3016B	0.0	0.0	0.0	0.0
1N4141	0.0	0.0	0.0	0.0
1002	0.0	0.0	0.0	0.0
2N2857(C-B)	0.0	0.3067	0.6978	0.5076
2N2857(E-B)	0.0	0.3067	0.6978	0.5076
2N3375(C-B)	1.5526	0.0	0.0	0.0
2N3375(E-B)	0.0	0.1190	0.0	0.0
2N1490:JAN(C-B)	0.0	1.8736	0.0	0.0
2N1490:JAN(E-B)	0.0	1.8278	0.0	0.0
2N3584(C-B)	0.2236	0.0	0.0	0.0
2N3584(E-B)	0.0	0.3401	0.0	0.0
2N2894(C-B)	0.0	2.0135	0.0	0.0
2N2894(E-B)	0.0	0.1206	0.0	0.0
2N2894(C-B)	0.0	0.5254	0.0	0.0
2N5829(C-B)	0.0	0.1511	0.2877	0.2505
2N5829(E-B)	0.0	0.4358	0.0	0.0
2N3013:JAN(C-B)	0.0	0.392	0.0	0.0
2N3013:JAN(E-B)	0.0	0.7067	0.0	0.0
CA3018(C-B)	0.0	0.1438	0.0	0.0
CA3018(E-B)	7.8696	0.0	0.0	0.0
2N1613:JAN(C-B)	0.0	11.8843	16.2980	18.6519
2N1613:JAN(E-B)	0.0	4.2389	0.0	0.0
2N1485:JAN(C-B)	1.5216	2.3543	0.0	0.0
2N1485:JAN(E-B)	0.0	29.8507	0.0	0.0
2N3439(C-B)	0.1311	0.0	0.0	0.0
2N3439(E-B)	0.0	0.0933	0.0	0.0
2N706:JAN(C-B)	0.0	2.8335	0.0	4.3832
2N706:JAN(E-B)	0.0	0.0	0.0	0.0
1N2580	2.9173	0.0	0.0	0.0
1N751A:JAN	0.0	0.0	0.0	0.0
1N6850:JAN	1.5861	0.0	0.0	0.0
1N2991:JAN	0.0	3.6068	0.0	0.0
1N3025:JAN	0.0	1.0632	0.0	0.0
M01056	0.0	0.0266	0.0	0.0
1N746A:JAN	0.0	1.4103	0.0	0.0
1N645:JAN	4.8762	1.6311	0.0	0.0
1N1202A:JAN	0.0	0.0	0.0	0.0
1N1731:JAN	11.5525	0.0	0.0	0.0

1.59	33.33	1.58	31.67	1.58	30.00	1.55	28.33	1.53	26.67
1.52	25.00	1.45	23.33	1.45	21.67	1.43	20.00	1.34	16.33
1.32	16.67	1.25	15.00	1.25	13.33	1.23	11.67	1.14	10.00
1.08	8.33	1.07	6.67	1.06	5.00	1.03	3.33	1.02	1.67
0.0	0.0								
279.25	100.00	231.36	99.28	96.10	98.55	91.35	97.83	40.72	97.10
29.85	96.38	25.50	95.65	21.36	94.93	16.51	94.20	13.74	93.48
12.55	92.15	12.03	92.03	11.88	91.50	10.97	90.58	10.90	89.86
10.79	89.13	10.72	88.61	10.63	87.68	8.78	86.96	8.61	86.23
8.59	85.51	8.45	84.78	8.40	84.06	8.37	83.33	8.29	82.61
7.99	81.88	7.61	81.16	7.56	80.43	7.39	79.71	7.36	78.99
7.34	78.26	6.95	77.54	6.83	76.81	6.62	76.09	6.54	75.36
6.38	74.64	6.36	73.91	6.30	73.19	6.19	72.46	6.13	71.74
6.13	71.01	6.01	70.29	5.66	69.57	5.64	68.84	5.58	68.12
5.44	67.39	5.20	66.67	4.74	65.94	4.49	65.22	4.33	64.49
4.24	63.77	4.11	63.04	4.09	62.42	3.85	61.59	3.80	60.87
3.66	60.14	3.61	59.42	3.61	58.70	3.60	57.97	3.46	57.25
3.37	56.52	3.34	55.80	3.36	55.07	3.26	54.35	3.18	53.62
3.12	52.90	3.11	52.17	3.09	51.15	3.06	50.42	3.02	50.00
2.95	49.28	2.94	48.55	2.94	47.83	2.92	47.10	2.85	46.38
2.84	45.65	2.83	44.93	2.83	44.20	2.79	43.48	2.72	42.75
2.69	42.03	2.66	41.40	2.56	40.58	2.44	39.86	2.44	39.13
2.44	38.41	2.35	37.68	2.29	36.96	2.23	36.23	2.13	35.51
2.10	34.78	2.04	34.06	2.01	33.33	1.99	32.61	1.93	31.88
1.90	31.16	1.89	30.43	1.89	29.71	1.87	28.99	1.83	28.26
1.82	27.54	1.77	26.81	1.77	26.09	1.77	25.36	1.75	24.64
1.73	23.91	1.72	23.19	1.68	22.46	1.67	21.74	1.67	21.01
1.63	20.29	1.63	19.57	1.60	18.84	1.60	18.12	1.54	17.39
1.53	16.67	1.50	15.94	1.48	15.22	1.43	14.49	1.41	13.77
1.40	13.04	1.36	12.32	1.32	11.59	1.31	10.77	1.26	10.14
1.26	9.42	1.26	8.70	1.18	7.97	1.18	7.25	1.17	6.52
1.12	5.80	1.11	5.07	1.11	4.35	1.11	3.62	1.08	2.90
1.06	2.17	1.06	1.43	1.03	0.72	0.72	0.0	0.0	0.0
29.63	100.00	24.64	97.78	22.59	95.56	22.33	93.33	20.05	91.11
16.30	88.89	10.44	86.67	9.95	84.44	9.31	82.12	7.73	80.00
6.44	77.78	6.04	75.56	4.44	73.33	4.37	71.11	4.28	68.89
4.12	66.67	3.86	64.44	3.73	62.22	3.51	60.00	3.48	57.78
3.23	55.56	3.08	53.33	2.94	51.11	2.86	48.9	2.66	46.67
2.65	44.44	2.62	42.22	2.61	40.00	2.26	37.78	2.24	35.56
2.16	33.33	2.13	31.11	2.13	28.89	2.08	26.67	1.92	24.44
1.79	22.22	1.79	20.00	1.72	17.78	1.67	15.56	1.50	13.33
1.48	11.11	1.43	8.89	1.34	6.67	1.20	4.44	1.08	2.22
0.0	0.0								
228.12	130.00	104.34	98.41	74.63	96.83	32.99	95.24	24.39	93.65
19.78	92.06	18.65	90.48	12.96	88.69	10.66	87.30	10.43	85.71
10.30	84.13	8.85	82.54	7.41	80.95	6.89	79.37	6.55	77.78
5.95	76.19	5.36	74.60	5.10	73.02	4.98	71.43	4.83	69.44
4.77	68.25	4.58	66.67	4.45	65.08	4.38	63.49	4.37	61.90
4.26	60.32	4.02	58.73	3.99	57.14	3.90	55.56	3.72	53.97
3.59	52.38	3.39	50.79	3.36	49.21	3.32	47.62	3.24	46.13
3.23	44.44	3.23	42.86	3.18	41.27	3.16	39.68	3.08	38.10

APPENDIX A

2.99	36.51	2.99	34.92	2.97	33.33	2.96	31.75	2.94	30.16
2.82	28.57	2.73	26.98	2.55	25.40	2.53	23.81	2.43	22.22
2.33	20.63	2.31	19.05	2.30	17.46	2.05	15.87	2.04	14.79
1.97	12.70	1.94	11.11	1.82	9.52	1.79	7.94	1.73	6.35
1.13	4.76	1.05	3.17	1.02	1.59	0.0	0.0	0.0	0.0
0.0	0.0								

RATIO OF EXPERIMENTAL AND PREDICTED POWER TO DAMAGE VS PERCENTAGE CONFIDENCE LEVEL FOR AVERAGE VALUE OF FIVE PRIORITY MODELS

253.68	100.00	231.38	99.39	96.10	98.79	82.99	98.18	66.88	97.58
59.05	96.97	40.72	96.36	27.12	95.76	21.15	95.15	19.91	94.55
18.67	93.94	15.61	93.33	15.37	92.13	14.17	92.12	12.81	91.52
12.65	90.91	11.76	90.30	11.61	89.70	11.55	89.09	10.74	88.48
10.65	87.88	10.63	87.27	10.52	86.47	10.37	86.06	9.95	85.45
9.17	84.85	9.13	84.24	8.88	83.64	8.23	83.03	7.41	82.42
7.25	81.82	7.17	81.21	7.04	80.41	6.78	80.00	6.76	79.39
6.71	78.79	6.69	78.18	6.62	77.58	6.61	76.97	6.56	76.36
6.54	75.76	6.47	75.15	6.36	74.55	6.18	73.94	6.00	73.33
5.99	72.73	5.51	72.12	5.44	71.52	5.42	70.91	5.24	70.30
5.04	69.70	4.98	69.09	4.90	68.48	4.78	67.86	4.70	67.27
4.68	66.67	4.68	66.06	4.46	65.45	4.41	64.85	4.33	64.24
4.33	63.64	4.17	63.03	4.15	62.42	4.12	61.82	4.11	61.21
3.88	60.61	3.88	60.00	3.80	59.39	3.71	58.79	3.71	58.18
3.66	57.58	3.61	56.97	3.61	56.36	3.61	55.76	3.60	55.15
3.57	54.55	3.54	53.94	3.52	53.33	3.37	52.73	3.36	52.12
3.35	51.52	3.25	50.91	3.21	50.30	3.08	49.70	3.01	49.09
2.98	48.48	2.95	47.88	2.92	47.27	2.92	46.67	2.92	46.06
2.90	45.45	2.88	44.85	2.83	44.24	2.79	43.64	2.75	43.03
2.72	42.42	2.71	41.82	2.70	41.21	2.70	40.61	2.69	40.00
2.66	39.39	2.63	38.79	2.56	38.18	2.44	37.58	2.44	36.97
2.44	36.36	2.43	35.76	2.41	35.15	2.41	34.55	2.38	33.94
2.33	33.33	2.30	32.73	2.29	32.12	2.24	31.52	2.24	30.91
2.23	30.30	2.22	29.70	2.21	29.19	2.19	28.58	2.13	27.88
2.11	27.27	2.10	26.67	2.10	26.06	2.08	25.45	2.02	24.85
2.00	24.24	1.98	23.64	1.98	23.03	1.94	22.42	1.93	21.82
1.92	21.21	1.89	20.61	1.86	20.00	1.82	19.39	1.80	18.79
1.79	18.18	1.78	17.58	1.77	16.97	1.74	16.36	1.73	15.76
1.72	15.15	1.71	14.55	1.67	13.94	1.67	13.33	1.67	12.73
1.65	12.12	1.64	11.52	1.64	10.91	1.61	10.30	1.61	9.70
1.60	9.09	1.60	8.48	1.57	7.86	1.54	7.27	1.54	6.67

1.40	6.06	1.35	5.45	1.32	4.85	1.25	4.24	1.12	3.64
1.11	3.03	1.10	2.62	1.08	1.82	1.06	1.21	1.03	0.61
0.0	0.0								

ARITHMETIC MEAN OF ABOVE DATA = 9.44

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